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# Energy error based numerical algorithms for Cauchy problems for nonlinear elliptic or time dependent operators

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# Overview

1. A variant of the Cauchy Problem and its applications
2. Solution of the CP by splitting of fields and energy-like error minimization
3. The pseudo-energy for various kind of operators
4. Numerical examples



# The Cauchy problem ... and its applications

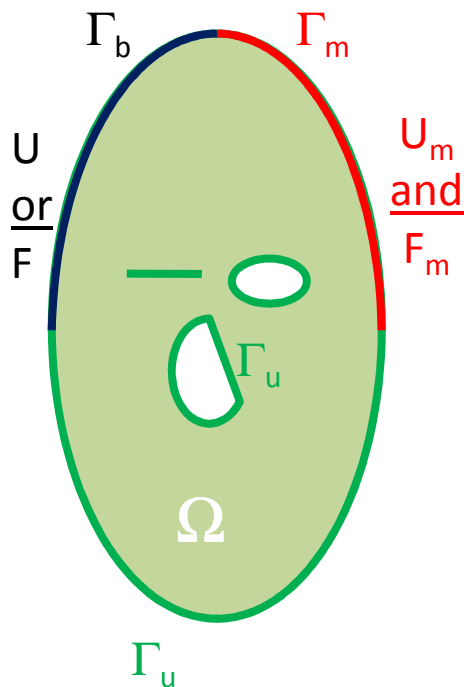
## ○ A variant of the Cauchy problem :

### ◆ Basic ingredients :

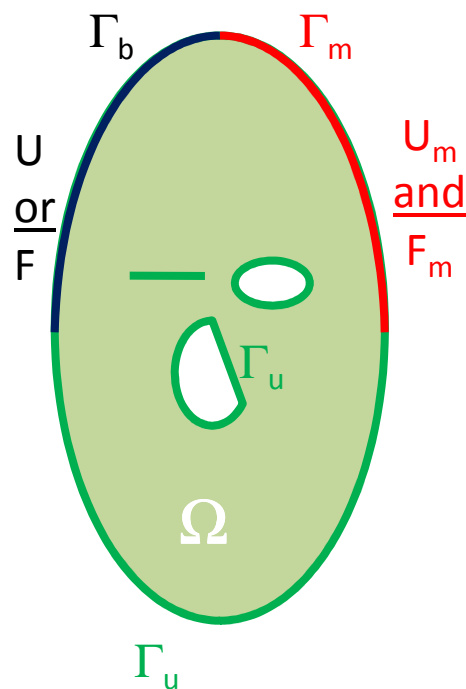
- A Domain  $\Omega$  of  $\mathbb{R}^n$  and eventually a time interval  $]0, D[$
- A PDO  $A$  acting on a field  $u$  defined on  $\Omega \times ]0, D[$  or  $\Omega$
- A boundary operator  $B$  associated with  $A$
- A part  $\Gamma_m$  of the boundary of  $\Omega$  ( $\partial\Omega = \Gamma_m \cup \Gamma_u \cup \Gamma_b$ )
- A field  $f$  or  $U$  given on  $\Gamma_b \times ]0, D[$  or  $\Gamma_b$
- A pair of fields given on  $\Gamma_m$  :  $(U_m, F_m)$

### ◆ The Cauchy problem : Find $u$ in $\Omega \times ]0, D[$ or $\Omega$ s.t. :

- $Au=0$  in  $\Omega \times ]0, D[$  or  $\Omega$
- $Bu=f$  or  $u=U$  on  $\Gamma_b \times ]0, D[$  or  $\Gamma_b$  (usual BC)
- $u=U_m$  and  $Bu= F_m$  on  $\Gamma_m \times ]0, D[$  or  $G_m$  (overspecified BC)



# The Cauchy problem ... and its applications

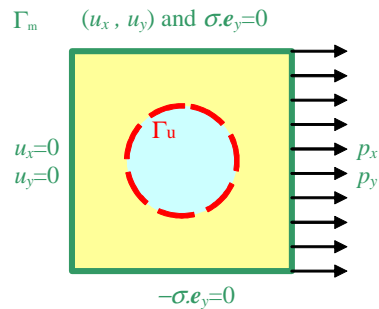


- The  $\Gamma_u$  part of the boundary is not accessible, and no BC is known. The Cauchy problem is then viewed
  - ◆ as a field extension problem into the domain : determine the whole field  $u$  inside the body from the knowledge of overspecified data on a part of its boundary.
  - ◆ as a data completion problem or a BC identification problem: find  $Bu$  and  $u$  on  $\Gamma_u$  from the knowledge of overspecified
  
- The second version shows that the Cauchy problem for bounded domains pertains to the field of inverse or identification problems.
  
- The Cauchy problem is the way of setting well-posed time evolution problems (hyperbolic or parabolic ones with  $\Gamma_u = \Omega$ ) but is ill-posed for others operators and/or others varieties  $\Gamma_u$

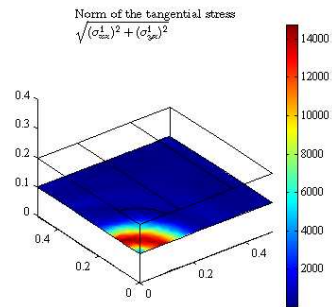


# Applications : Elliptic operators

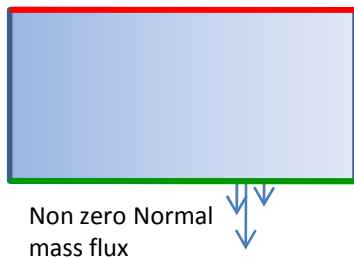
Thermal conduction, Elasticity , Stokes or Darcy system



Determination of elastic parameters for an inclusion with known position and geometry

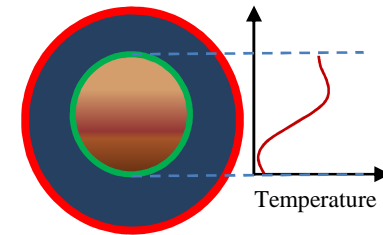


Evaluation of interface stresses

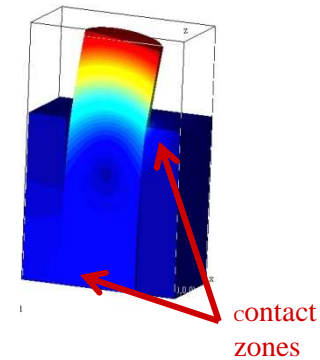


Determination of leakage in a Darcy system

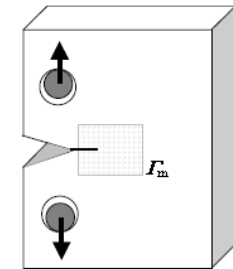
Identification of fluid stratification within a pipe



Identification of contact zone and pressure



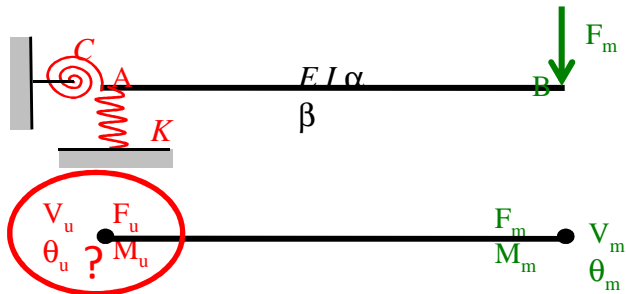
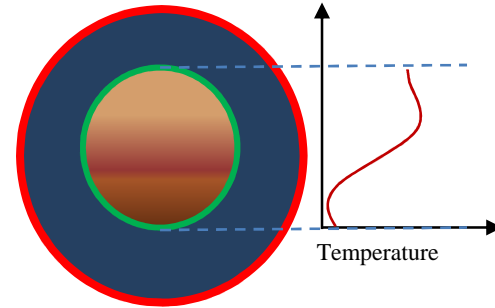
Determination of linear fracture mechanics parameters from external surface measurements



*Note that the relation between the boundary terms on  $\Gamma_u$  can be highly non linear*

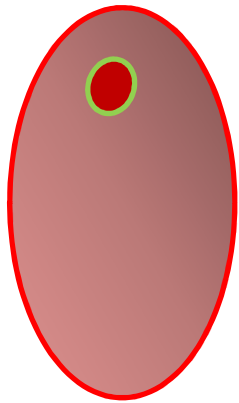
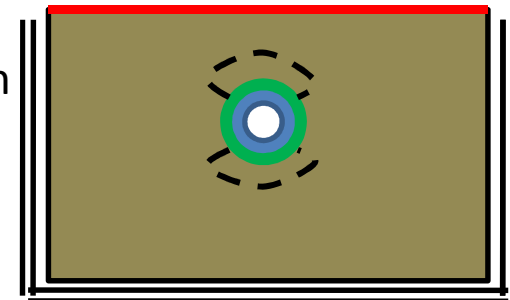
Applications : time dependant, non linear operators  
 Heat equation, Elastodynamics, Stokes system, hyperelasticity

Identification of fluid stratification evolution within a pipe



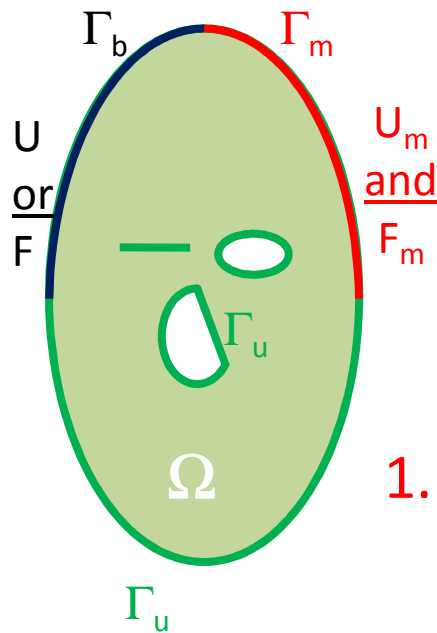
Identification of varying BC for a structure

Determination of traction zones in a non linear elastic medium around a tunnel and identification contact zone at the interfaces



Determination physical characteristics of an inclusion with known shape and position for non linear incompressible media

# Solution of the CP by splitting the fields and a (pseudo) energy error minimization



## Two simple ideas

Model Problem :  
the Laplace operator

$$\begin{cases} \Delta u = 0 & \text{in } \Omega \\ \nabla u \cdot n = 0 & \text{on } \Gamma_b \\ u = U_m, \nabla u \cdot n = F_m & \text{on } \Gamma_m \\ u = \tau, \nabla u \cdot n = \eta & \text{on } \Gamma_u \end{cases}$$

1. Introduce the BC on  $\Gamma_u$  as unknowns and define two solutions of well-posed problems, using one of the overspecified BC on  $\Gamma_m$  and one of the lacking BC on  $\Gamma_u$

$$\begin{cases} \Delta u_1 = 0 & \text{in } \Omega \\ \nabla u_1 \cdot n = 0 & \text{on } \Gamma_b \\ u_1 = U_m & \text{on } \Gamma_m \\ \nabla u_1 \cdot n = \eta & \text{on } \Gamma_u \end{cases}$$

Unknowns :  
 $\eta$  and  $\tau$

$$\begin{cases} \Delta u_2 = 0 & \text{in } \Omega \\ \nabla u_2 \cdot n = 0 & \text{on } \Gamma_b \\ \nabla u_2 \cdot n = F_m & \text{on } \Gamma_m \\ u_2 = \tau & \text{on } \Gamma_u \end{cases}$$



# Solution of the CP by splitting the fields and a (pseudo) energy error minimization



If  $u_1$  and  $u_2$  are equal  
then the CP is solved :  $u = u_1$  and the BC on  $\Gamma_u$  are  $(\eta, \tau)$

2. Introduce a (semi) norm on  $(u_1 - u_2)$  and minimize it.

$$E(\eta, \tau) = \frac{1}{2} \int_{\Omega} (\nabla u_1(\eta) - \nabla u_2(\tau))^2 \quad \longrightarrow \quad (u|_{\Gamma_u}, \nabla u \cdot n|_{\Gamma_u}) = \underset{\eta, \tau}{\text{ArgMin}} E(\eta, \tau)$$

The Energy error  $E$  is closely related to the physics of the problem and is preferred to the usual least-square error (take into account the eventual heterogeneity, anisotropy .....





## Some nice properties of the (pseudo) energy error

- The Error energy is quadratic convex positive
- The minimum is zero (for compatible pair of data  $(U_m, F_m)$ )
- $E$  has an expression involving only boundary terms (used for computation):

$$E(\eta, \tau) = \frac{1}{2} \int_{\partial\Omega} (\nabla u_1(\eta) - \nabla u_2(\tau)) \cdot n (u_1(\eta) - u_2(\tau))$$

$$E(\eta, \tau) = \frac{1}{2} \int_{\Gamma_m} (\nabla u_1 \cdot n - F_m)(U_m - u_2) + \frac{1}{2} \int_{\Gamma_u} (\eta - \nabla u_2 \cdot n)(u_1 - \tau)$$

- The term energy is (abusively here) coined from the variational properties associated with the Laplace operator:



$$u = \underset{v}{\text{ArgMin}} \frac{1}{2} a(v, v) - l(v) \quad a(u, v) = \int_{\Omega} \nabla u \cdot \nabla v$$

# Practical implementation of the energy error method

- Use iterative minimization methods rather than first-order optimality conditions (as soon as the number of unknowns increases) : CG with trust region methods.
- Compute the gradient by (2) adjoint problems : Laplace problems with boundary terms only. Each iteration needs 4 resolutions of direct problems of same kind.
- The fixed-point two-steps algorithm of Kozlov-Maz'ya-Fomin (1991) can be interpreted as an alternating directions descent method for the minimization of  $E$  (*so that far better performances are achieved with a “serious” minimizing algorithm*)



# The pseudo-energy for various kind of operators : elliptic operators

- For linear elliptic symmetric operators, the pseudo energy as the same form as for the Laplace operator and uses the associated symmetric bilinear form :  $E(\eta, \tau) = a[u_1(\eta) - u_2(\tau), u_1(\eta) - u_2(\tau)]$

- For non-linear elliptic operator associated with a convex potential (like hyperelasticity)
 
$$\begin{cases} \operatorname{div} \sigma = 0 & \text{in } \Omega \\ \sigma \in \partial \varphi(\varepsilon), \varepsilon = \nabla u^s & \text{in } \Omega \\ \sigma(u) \cdot n = F_m, u = U_m & \text{on } \Gamma_m \end{cases}$$

- use the Fenchel cross-residual

$$E(\eta, \tau) = \int_{\Omega} (\sigma_1 - \sigma_2, \varepsilon(u_1) - \varepsilon(u_2)) d\Omega$$

*Reduces to the error energy for quadratic  $\varphi$*

$$E(\eta, \tau) \geq 0$$

$$E(\eta, \tau) = 0 \Leftrightarrow \sigma_1 \in \partial \varphi[\varepsilon(u_2)], \sigma_2 \in \partial \varphi[\varepsilon(u_1)]$$

*Then  $\varepsilon(u_2) = \varepsilon(u_1)$  if  $\varphi$  is differentiable*



# The pseudo-energy for various kind of operators : parabolic operators

- The model problem is the heat equation
 
$$\begin{cases} \rho c \dot{u} - \operatorname{div}(k \nabla u) = 0 & \text{in } \Omega \times ]0, D[ \\ u = U_m, k \frac{\partial u}{\partial n} = \Phi_m & \text{on } \Gamma_m \times ]0, D[ \\ u(x, 0) = u_0(x) & \text{in } \Omega \end{cases}$$

- The energy error is integrated over the time interval and a control on the final state (at  $t=D$ ) is introduced

$$E(\eta, \tau) = \int_0^D \int_{\Omega} k [\nabla (u_1 - u_2)]^2 d\Omega dt + \frac{1}{2} \int_{\Omega} \rho c [u_1 - u_2]_{t=D}^2 d\Omega$$

- The energy error enjoys again a boundary expression



$$E(\tau, \eta) = \int_0^D \int_{\Gamma_u} (u_1 - \tau)(\eta - k \nabla u_2 \cdot n) d\Gamma_u dt + \int_0^D \int_{\Gamma_m} (U_m - u_2)(k \nabla u_1 \cdot n - F_m) d\Gamma_m dt$$

# The pseudo-energy for various kind of operators : hyperbolic operators

- The model problem is the elastodynamics equation 
$$\begin{cases} \rho \ddot{u} + c \dot{u} - \operatorname{div}(\mathbf{A} : \boldsymbol{\varepsilon}(u) + \mathbf{B} : \boldsymbol{\varepsilon}(\dot{u})) = 0 & \text{in } \Omega \times ]0, D[ \\ [\mathbf{A} : \boldsymbol{\varepsilon}(u) + \mathbf{B} : \boldsymbol{\varepsilon}(\dot{u})] \cdot \mathbf{n} = F_m, u = U_m & \text{on } \Gamma_m \times ]0, D[ \end{cases}$$

$$u(x, 0) = u^0(x), \dot{u}(x, 0) = u^1(x) \text{ in } \Omega$$

- The energy error contains a control over the time interval of the dissipation, and a control on the final state (at  $t=D$ ) for the elastic and kinetic energies :

$$J(v) = \int_0^D \int_{\Omega} (c \dot{v}^2 + \mathbf{B} : \boldsymbol{\varepsilon}(\dot{v}) : \boldsymbol{\varepsilon}(\dot{v})) d\Omega dt + \frac{1}{2} \int_{\Omega} (\rho \dot{v}^2 + \mathbf{A} : \boldsymbol{\varepsilon}(v) : \boldsymbol{\varepsilon}(v)) d\Omega \Big|_{t=D}$$

$$E(\eta, \tau) = J[u_1(\eta) - u_2(\tau)]$$

- The energy error enjoys again a boundary expression



$$J(v) = \int_0^D \int_{\Gamma_m} (\mathbf{A} : \boldsymbol{\varepsilon}(v) + \mathbf{B} : \boldsymbol{\varepsilon}(\dot{v})) \cdot \dot{v} \cdot \mathbf{n} d\Gamma dt + \int_0^D \int_{\Gamma_u} (\mathbf{A} : \boldsymbol{\varepsilon}(v) + \mathbf{B} : \boldsymbol{\varepsilon}(\dot{v})) \cdot \dot{v} \cdot \mathbf{n} d\Gamma dt$$



## A remark for non dissipative media

- For purely elastic media ( $B=c=0$ ), the previous energy error degenerate into :

$$J(v) = \frac{1}{2} \int_{\Omega} (\rho \dot{v}^2 + A : \varepsilon(v) : \varepsilon(v)) d\Omega \Big|_{t=D}$$

- But due to the exact controllability of the elastodynamics equation (Lions, 1988) this error is no more sufficient :

$$J(v) = 0 \not\Rightarrow v = 0$$

- And a penalized energy must be employed ( $k, K$  pseudo material parameters) :

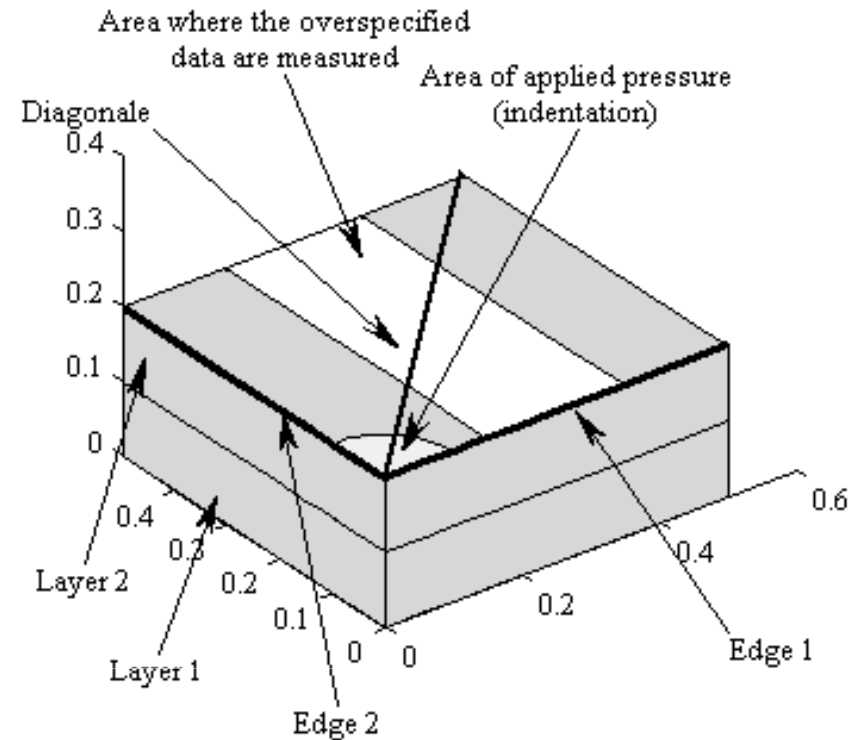
$$J(v) = \frac{1}{2} \int_{\Omega} (\rho \dot{v}^2 + A : \varepsilon(v) : \varepsilon(v)) d\Omega \Big|_{t=D} + \frac{\alpha}{2} \int_0^D \int_{\partial\Omega} (k v^2 + K \dot{v}^2) d\Gamma dt$$



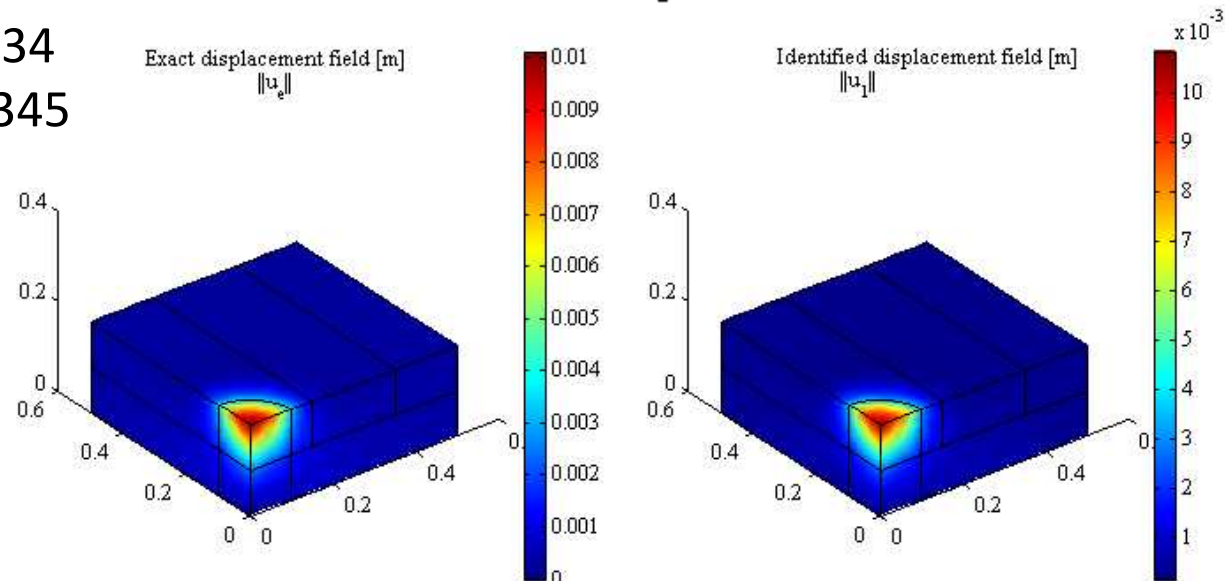
# Numerical examples

Indentation of an elastic bi-material :

- No information about the indentation force or indenter displacement
- “displacement field” measurements on a small part of the stress free surface
- Number of node on  $\Gamma_m$  : 134
- Number of nodes on  $\Gamma_u$  : 345
- 185 iterations

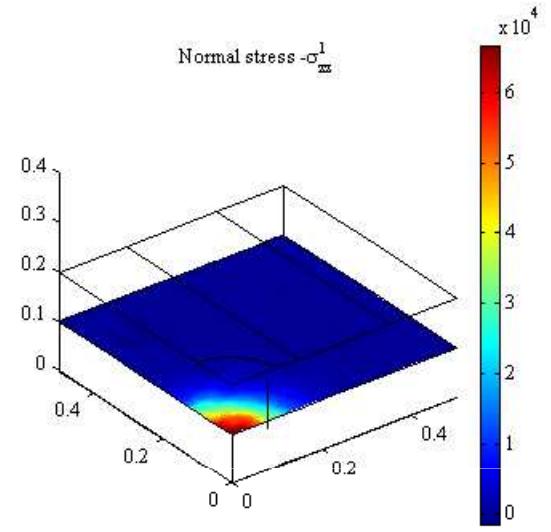
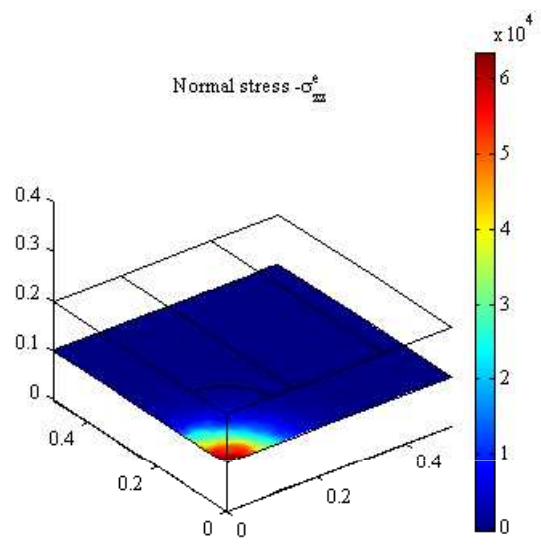


*Comparison of exact and identified displacement field*



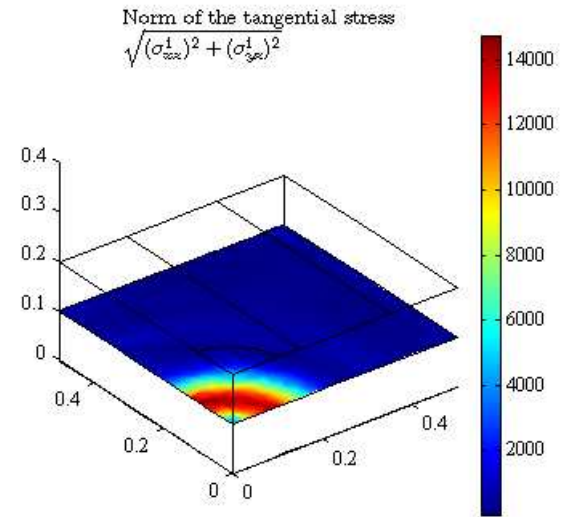
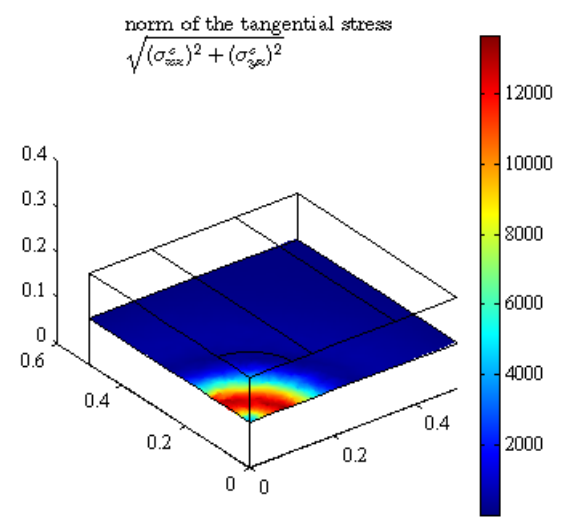
# Numerical Examples

## Indentation of an elastic bi-material



Comparison between identified and computed stress components on the interface

*Normal stresses*



*Norms of shear stresses*



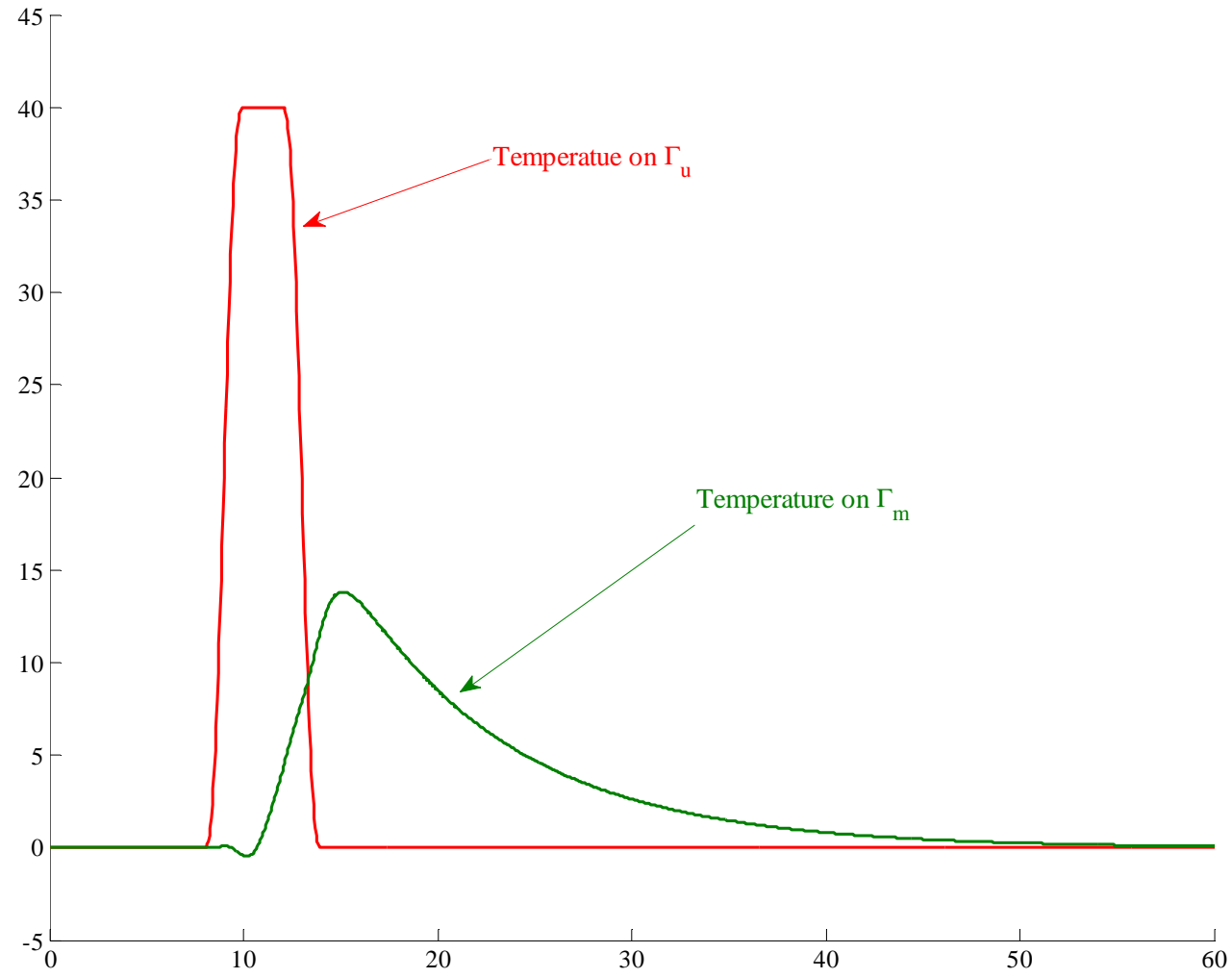
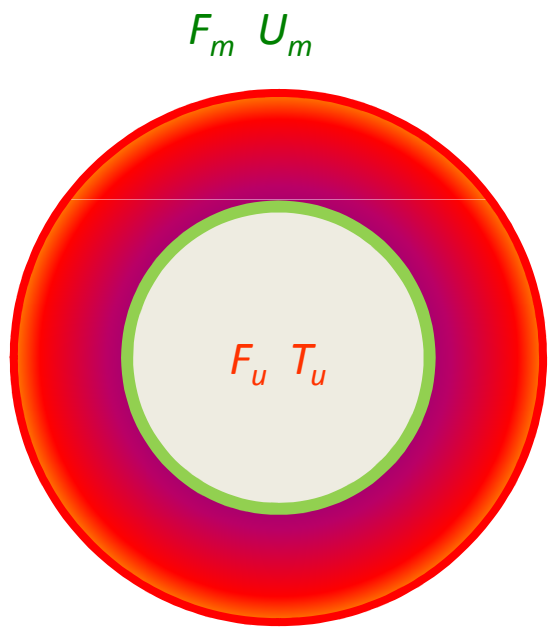


# Numerical Examples

Identification of inner temperature and heat flux in a pipe :  
heat equation

Two-dimensional model for pipeline :  
Inner radius  $R_i=12$  cm.  
Outer radius  $R_e = 12.92$  cm.

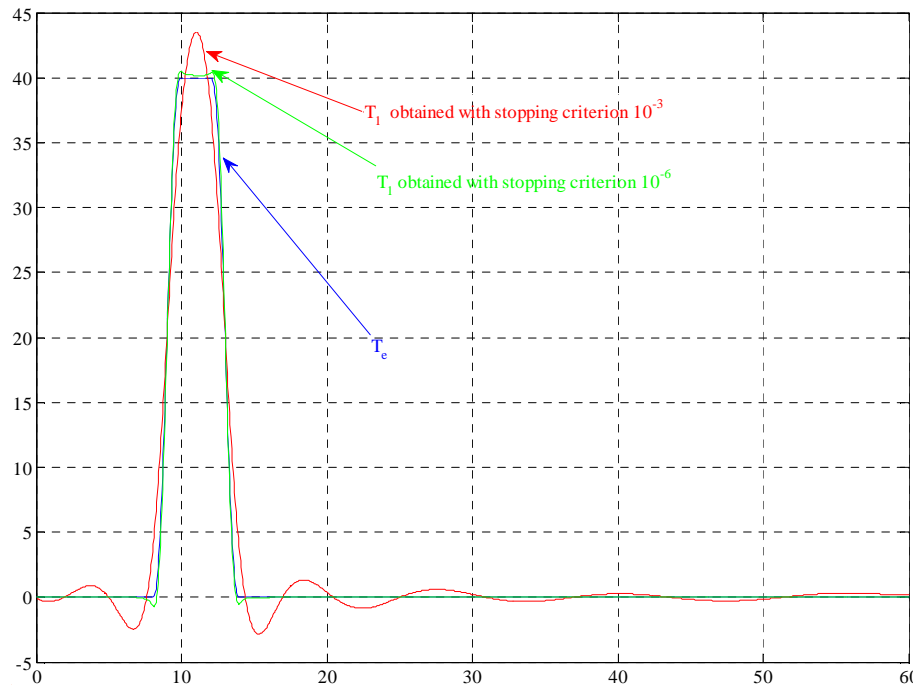
Material properties:  
 $k = 15.9 \times 10^{-2}$ ,  $\rho = 7.8 \times 10^{-3}$  Kg/cm<sup>3</sup>,  
 $c = 494$



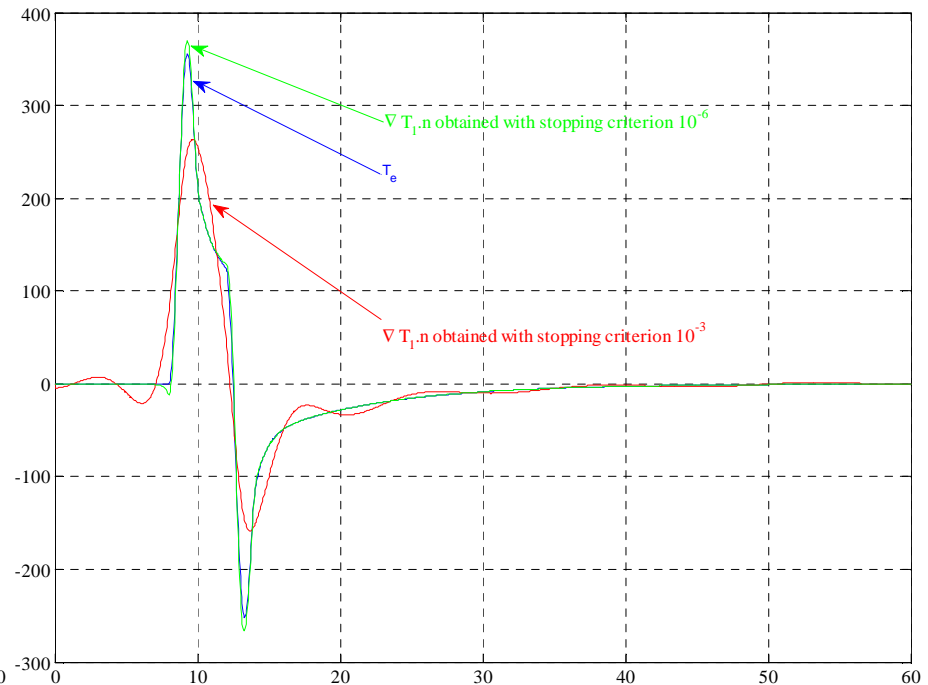
# Numerical Examples

Identification of inner temperature and heat flux in a pipe :  
heat equation

Influence of the stopping criterion



Comparison between identified  
and computed inner  
temperature

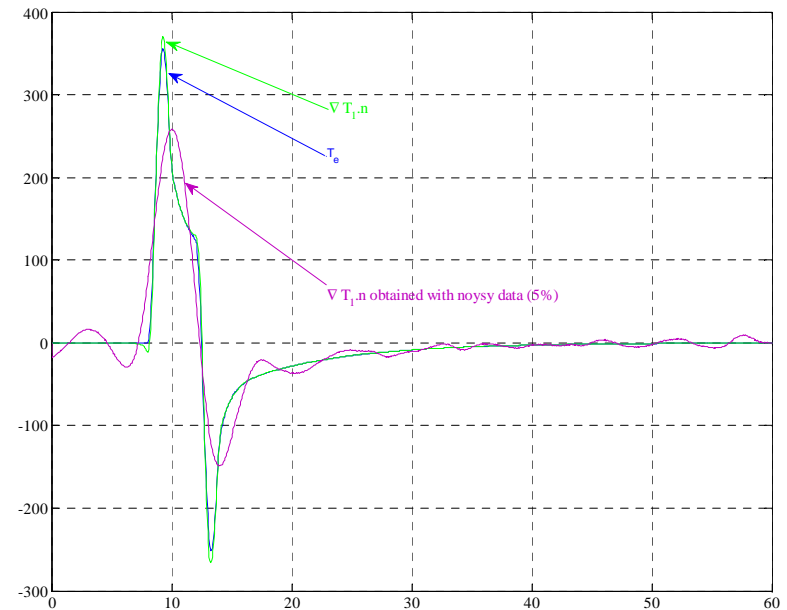
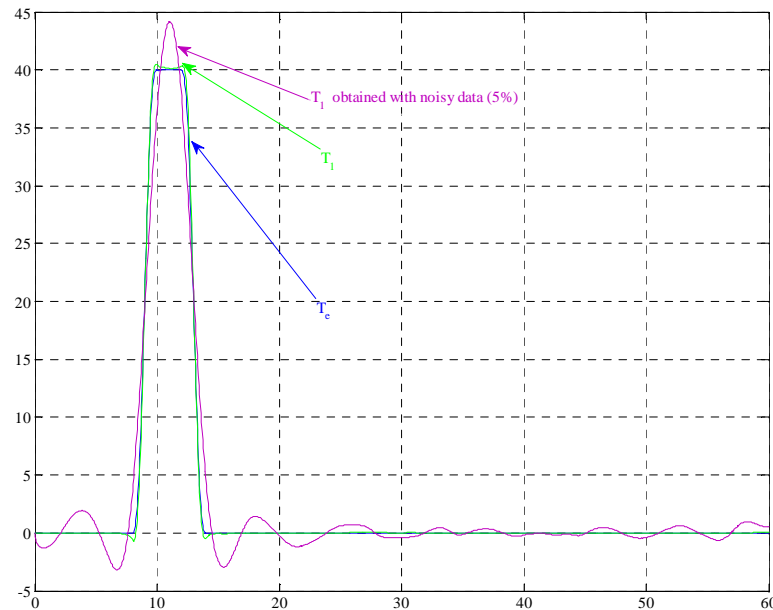
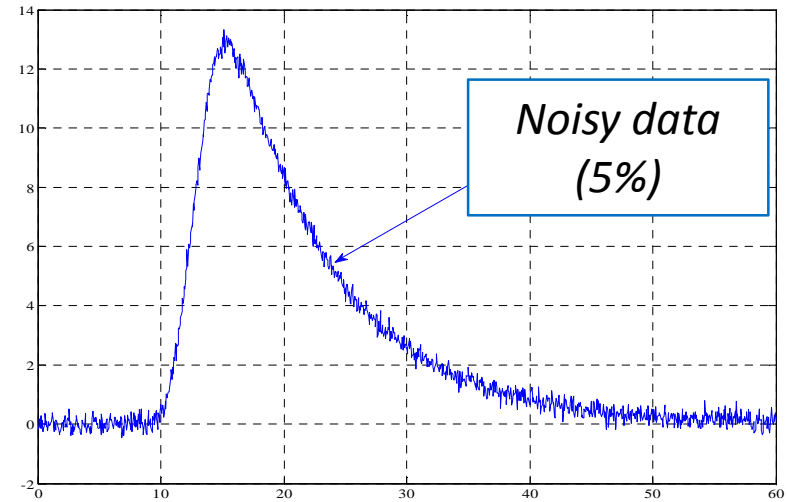


Comparison between identified  
and computed inner heat flux



# Numerical Examples

Identification of inner temperature and heat flux in a pipe :  
heat equation



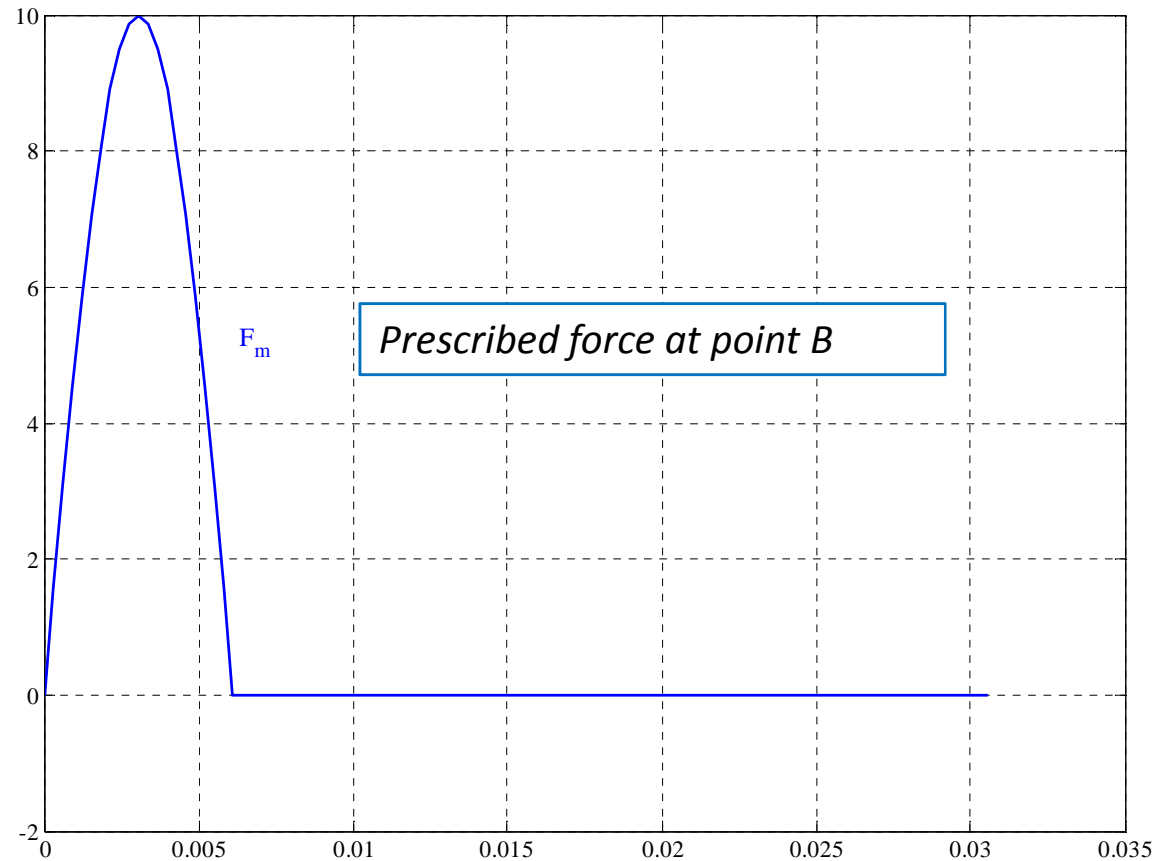
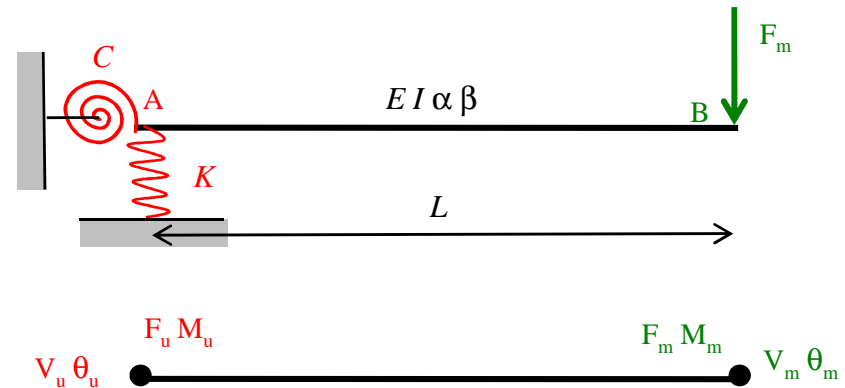
Comparison between identified  
and computed inner  
temperature



Comparison between identified  
and computed inner heat flux

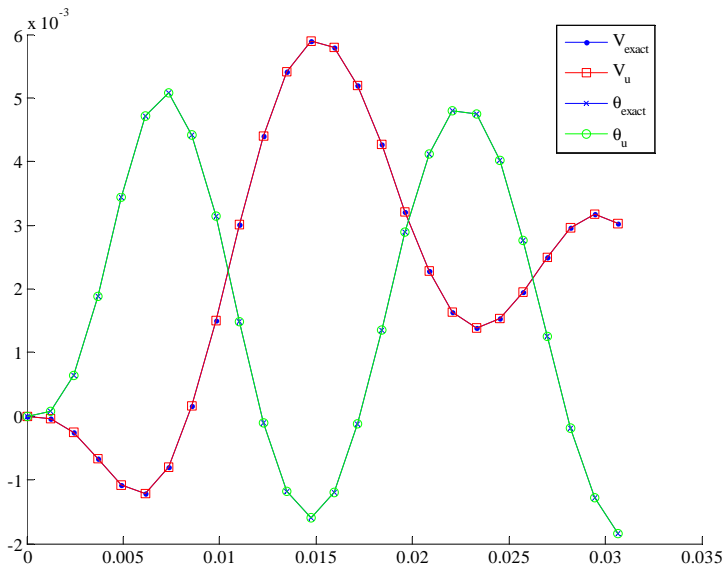
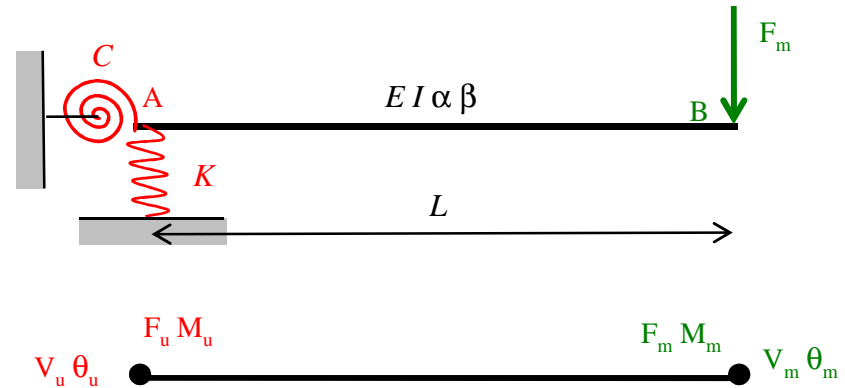
# Numerical Examples

Identification of BC for a beam under an impact loading : elastodynamics

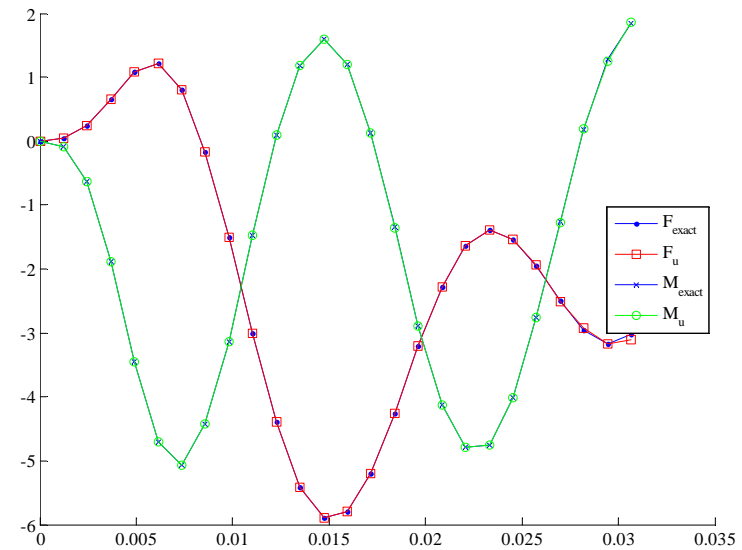


# Numerical Examples

Identification of BC for a beam under an impact loading : elastodynamics



Comparison between identified and computed displacement and rotation at point  $A$



Comparison between identified and computed moment and shear resultant at point  $A$



# Conclusions

- The method is quite general for (spatial) symmetric operators and lead to efficient functionals compared to least-squares based ones.
- It allows for dealing with 3D applications, and can be used with usual FEM softwares allowing monitoring procedures.
- Regularization is *a priori* needed (the CP is severely ill-posed) but with moderate noise it can be avoided because of smoothing behavior of the minimizing procedure and good behavior of the energy error functional
- Future work on computational efficiency, extension to non-symmetric operators, others applications and resolution of some troubles with adjoint techniques for time dependent and non-differentiable problems (non  $C^2$  convex potentials).

